

Thermal perturbations generated by near-surface electric discharges and mechanisms of their interaction with the airflow

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Outline

I. Background / Introduction

II. Kinetics of energy transfer and thermal perturbations in surface and volumetric ns pulse discharges

III. Effect of localized heating on formation of flow structures, implications for high-speed plasma flow control

IV. Effect of accelerated vibrational relaxation on nonequilibrium flow field, implications for high-speed flow control

V. Summary and future outlook

Plasma Flow Control Mechanisms and Challenges

I. EHD body force

- Coulomb force interaction in AC DBD discharges: neutral flow entrainment by ions. Low-speed boundary layer flow separation control.

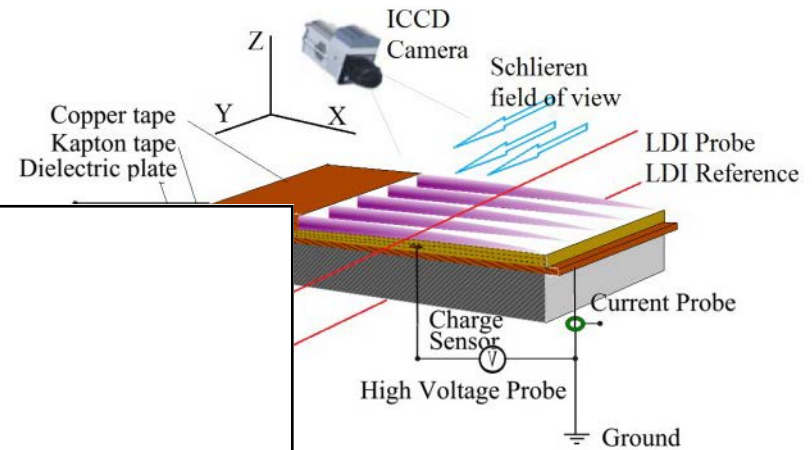
II. Repetitive Localized Heating

- Localized arc filament plasma actuators (LAFPA): inducing flow instabilities. Effective at low actuator powers, up to $M=0.9-2.0$
- Ns pulse surface plasma actuators (NS-DBD): coherent structures formation, boundary layer reattachment in low-temperature, ns pulse plasmas (up to $M=0.3$)

Goal

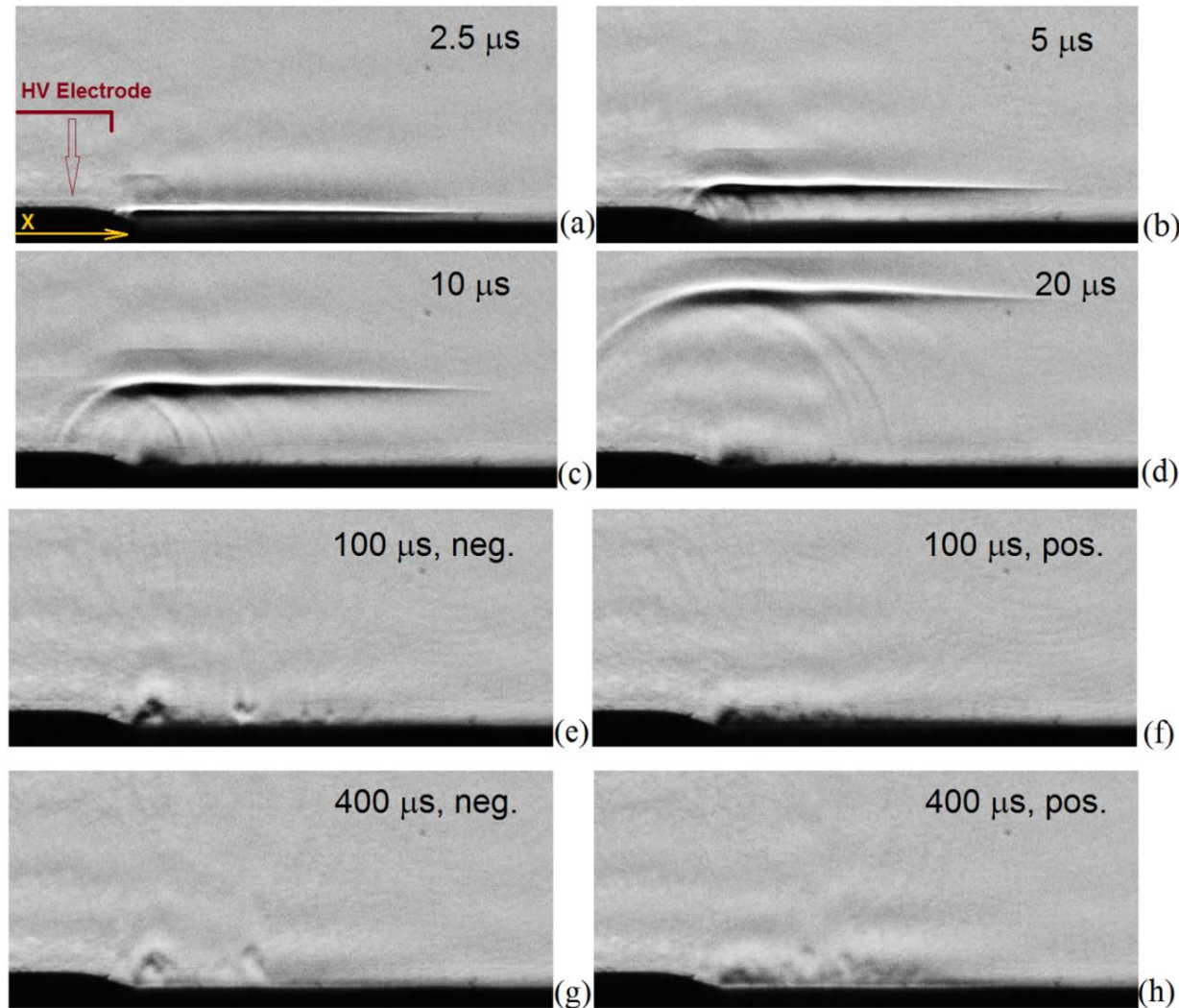
High-speed flow control at low energy cost, over a wide range of flow geometries, Mach and Re numbers: boundary layer transition and separation, shock wave control, drag reduction, mixing enhancement

Schlieren visualization of a NS-DBD plasma actuator operated in quiescent air



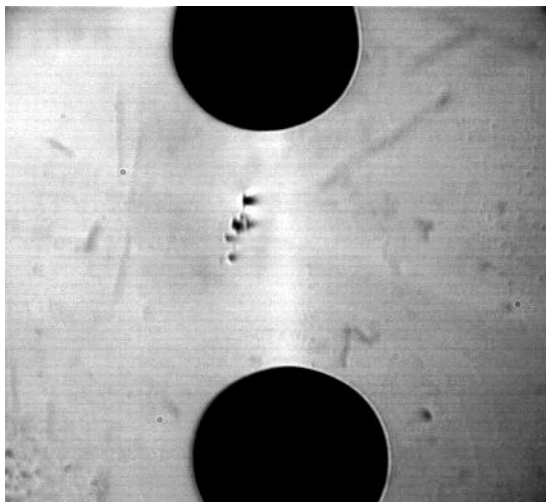
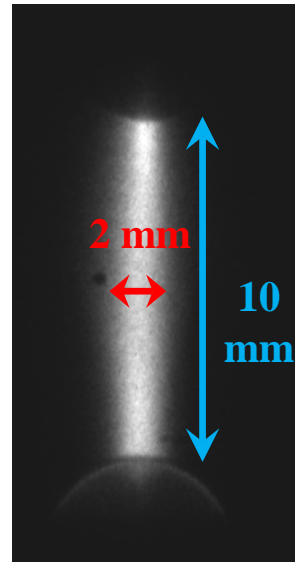
Schlieren visualization of a NS-DBD plasma actuator operated in quiescent air

Leonov et al, J. Phys. D: Appl. Phys., 2014

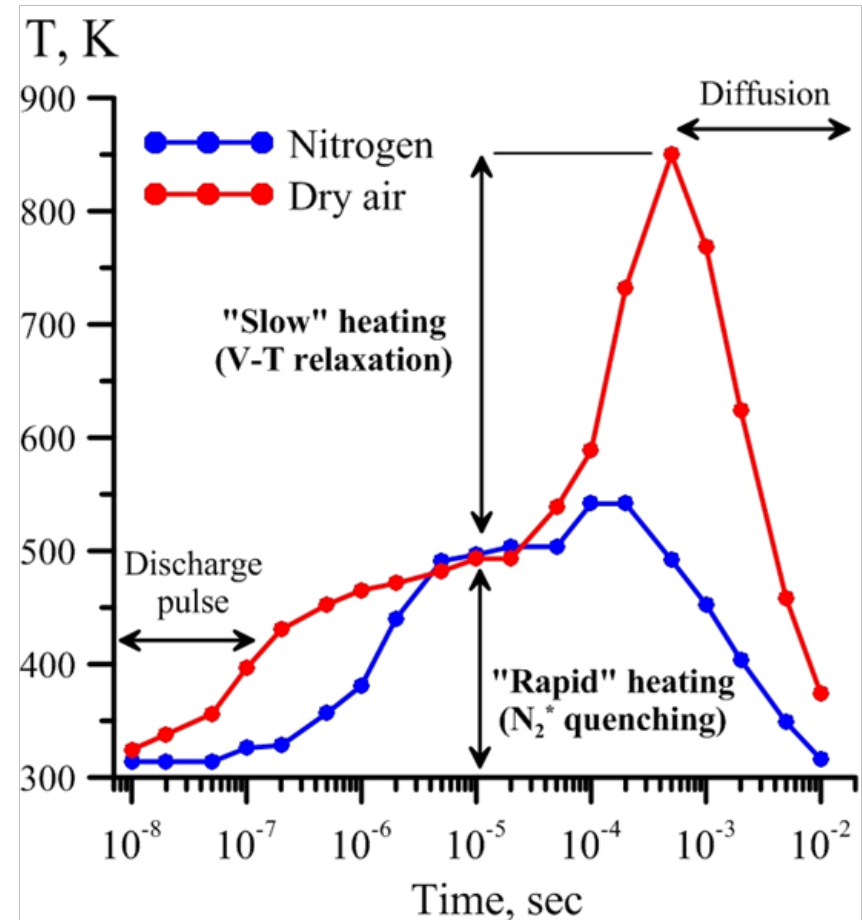


- Heating in the discharge: compression wave formation on μs time scale
- Residual heating: late small-scale random perturbations on $\sim 0.1\text{-}1$ ms time scale
- What are the kinetics involved? Which one is important for plasma flow control?

Temperature dynamics in volumetric ns pulse discharge filament in air (P=100 Torr)



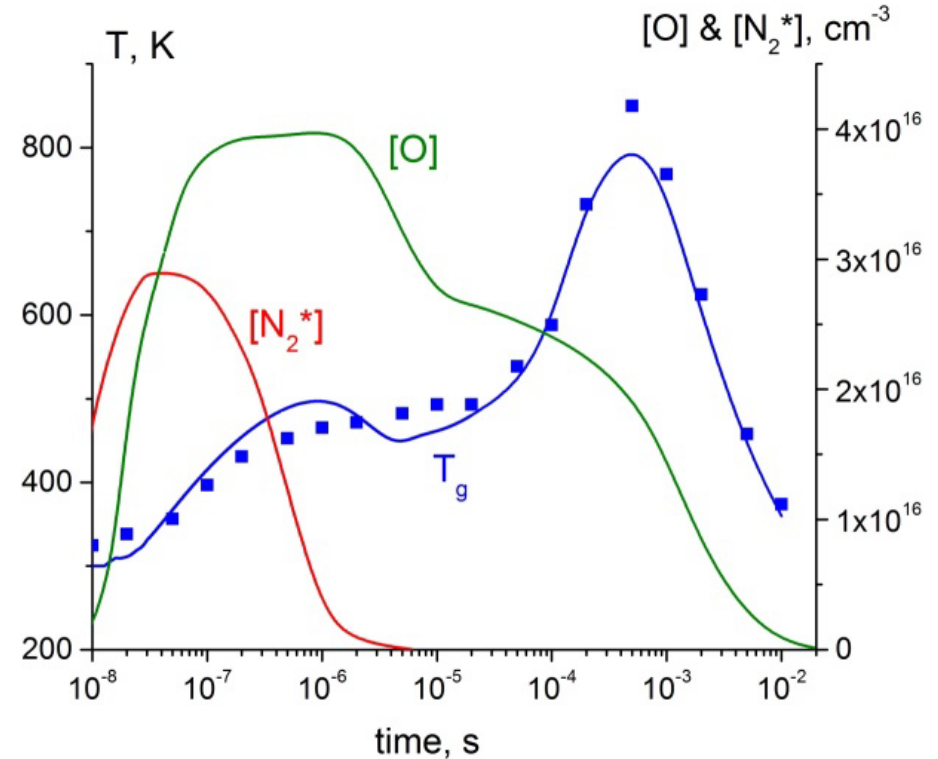
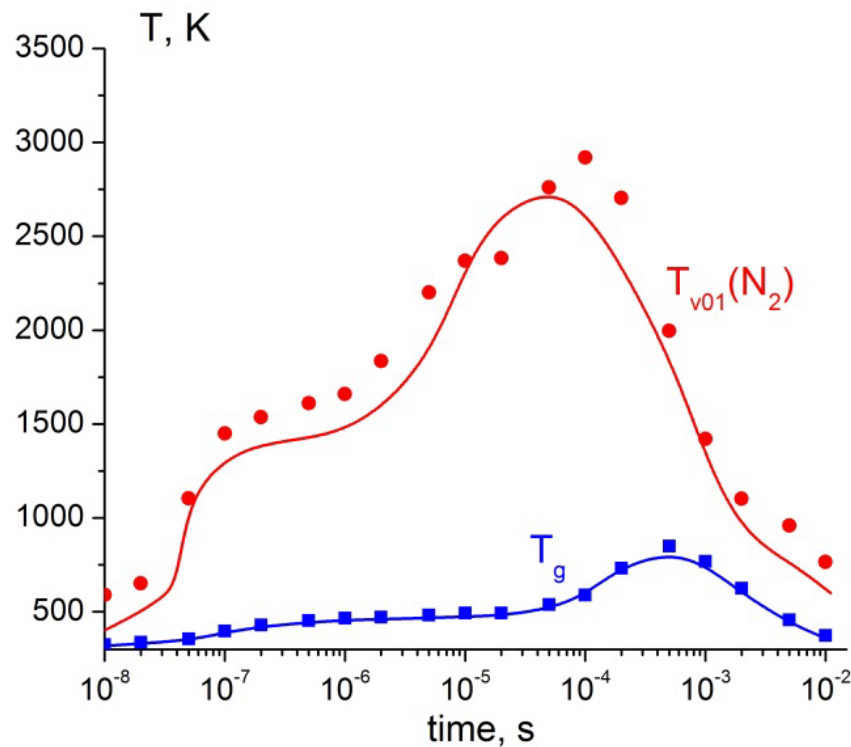
$t = 1-10 \mu\text{s}$ (frames are $1 \mu\text{s}$ apart)



Montello et al, J. Phys. D: Appl. Phys., 2012

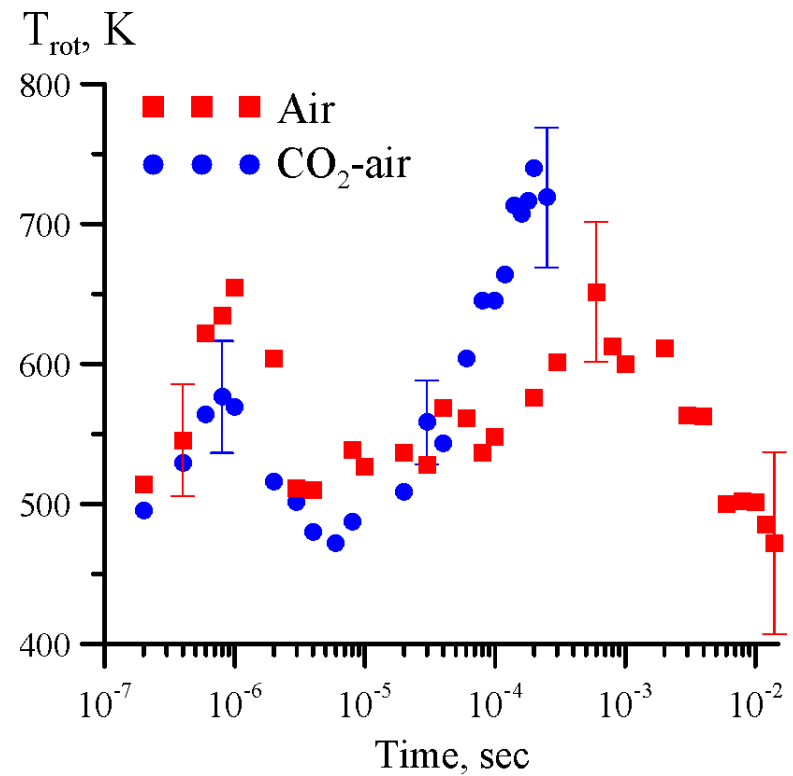
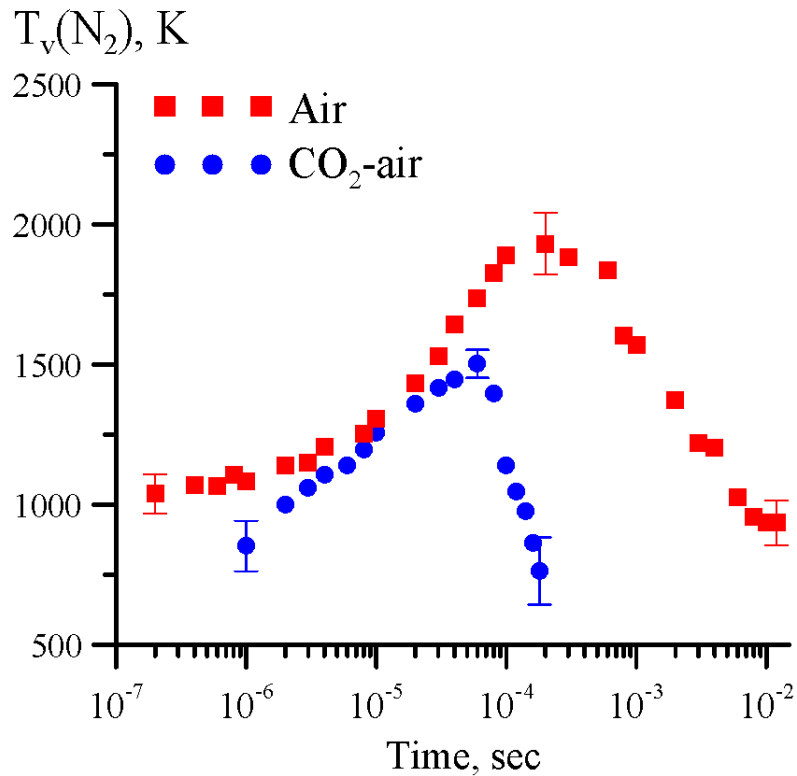
Montello et al, J. Fluid Science and Technol., 2013

Energy transfer and temperature dynamics in discharge and afterglow in air are well understood



- T_v rise in early afterglow: V-V exchange, $N_2(v) + N_2(v=0) \rightarrow N_2(v-1) + N_2(v=1)$
- T_v decay in late afterglow: V-T relaxation, $N_2(v) + O \rightarrow N_2(v-1) + O$
- “Rapid” heating: quenching of N_2 excited electronic states, $N_2^* + O_2 \rightarrow N_2(X) + O + O$
- “Rapid” heating: pressure overshoot on centerline, compression wave formation
- “Slow” heating: V-T relaxation, $N_2(X,v) + O \rightarrow N_2(X,v-1) + O$
- “Slow” heating: affecting “late” random perturbations”?

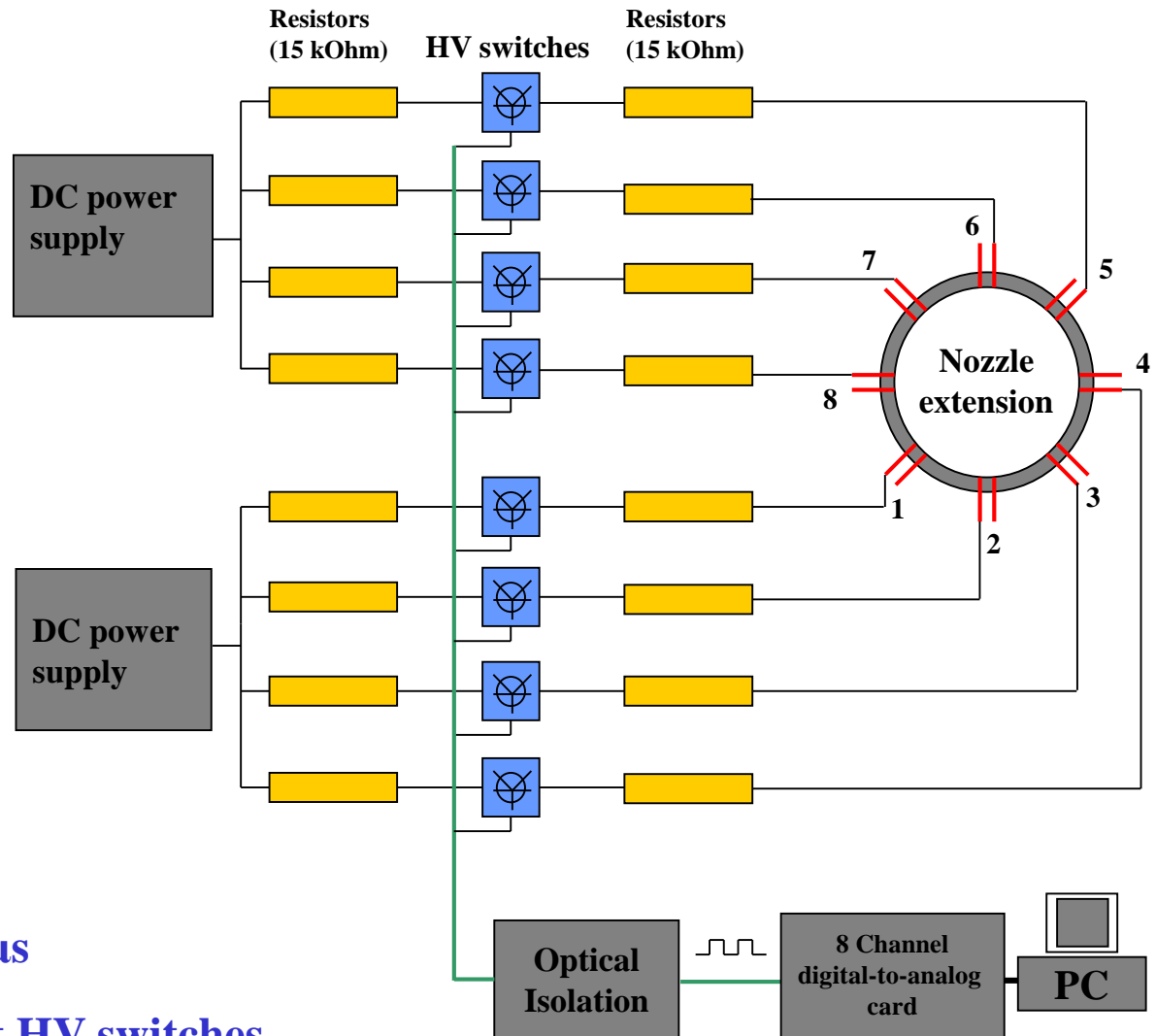
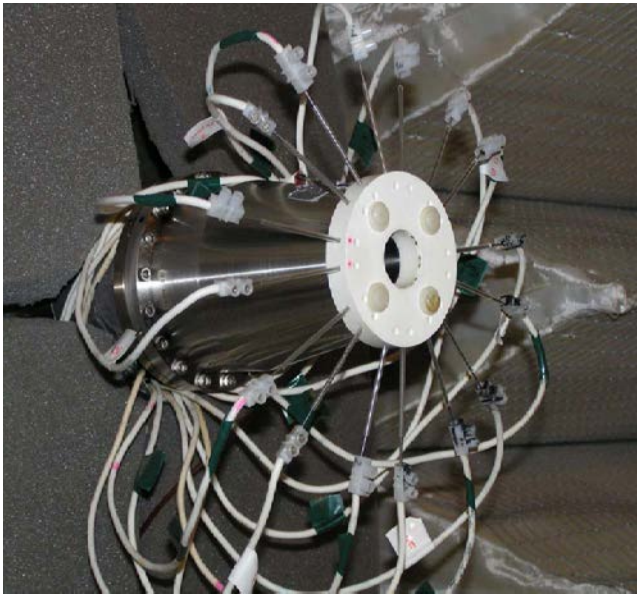
Adding CO₂ (efficient V-T relaxer) to air: accelerating “slow” heating rate



Mechanism of accelerated “slow” heating:

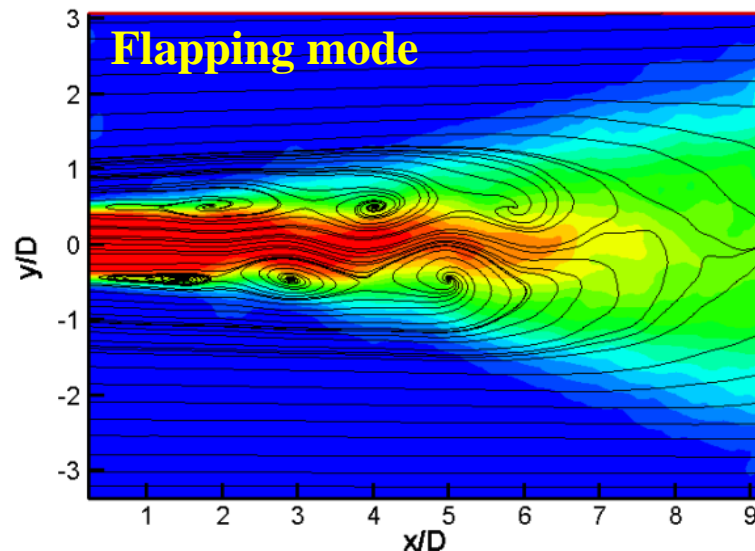
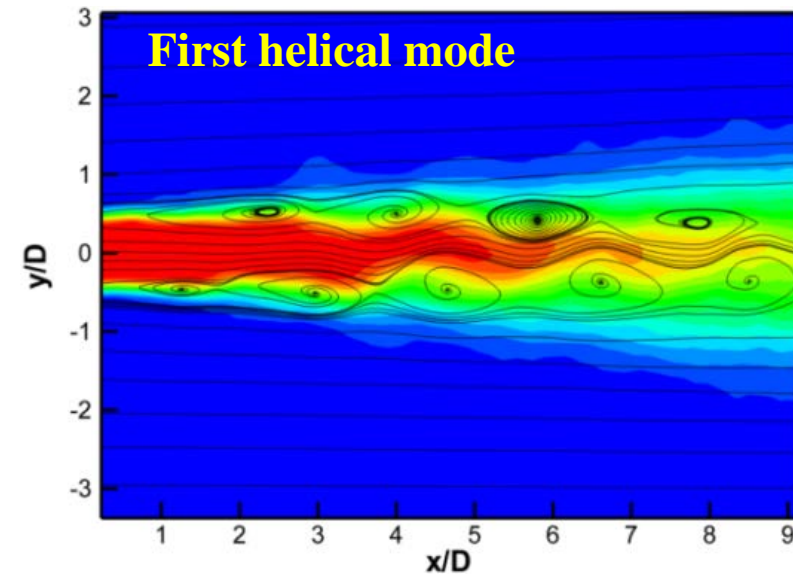
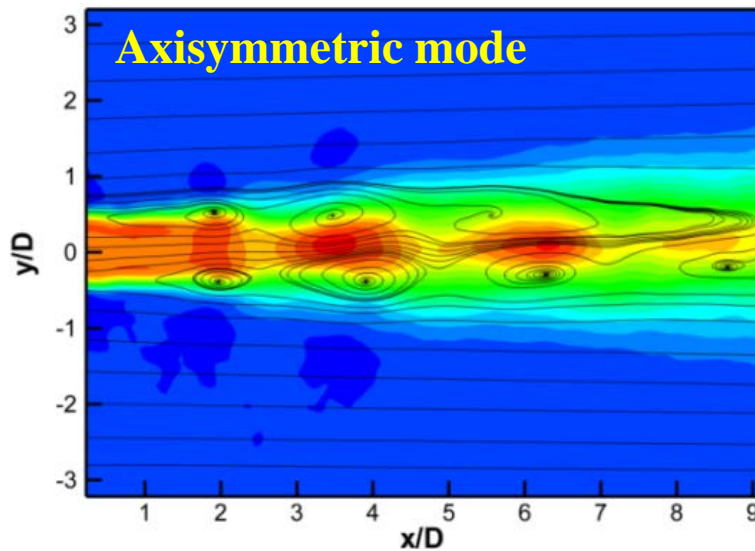
- V-V energy exchange between N₂ and CO₂(v₃) mode: $N_2(v=1) + CO_2(000) \leftrightarrow N_2(v=0) + CO_2(001)$
- CO₂ energy re-distribution among vibrational modes: $CO_2(001) + M \leftrightarrow CO_2(100,020,010) + M$
- V-T relaxation of bending mode: $CO_2(010) + M \rightarrow CO_2(100) + M$
- Heating by accelerated vibrational relaxation may be used for nonequilibrium flow control

Localized Arc Plasma Flow Actuators (LAPFA): Exciting instabilities in transonic and supersonic flows ($M=0.9-2.0$)



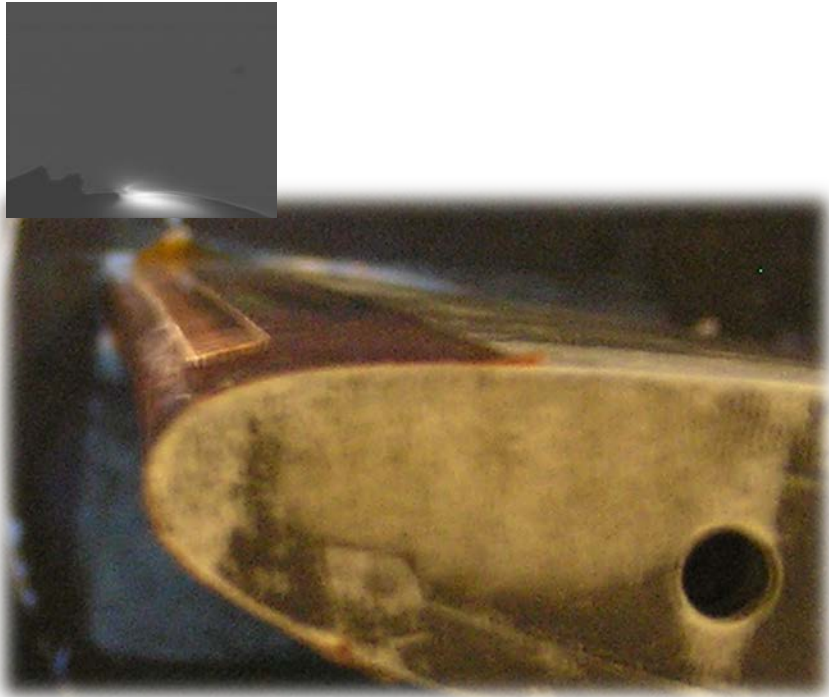
- Circular nozzle, 1 inch diameter
- Arc filament discharge pulses, $\sim 10 \mu s$
- Multiple channels controlled by fast HV switches
- Independent control of frequency, phase, and duty cycle \rightarrow excitation of different instability modes

LAPFA: Formation of spanwise vortices in a $M=0.9$ circular jet

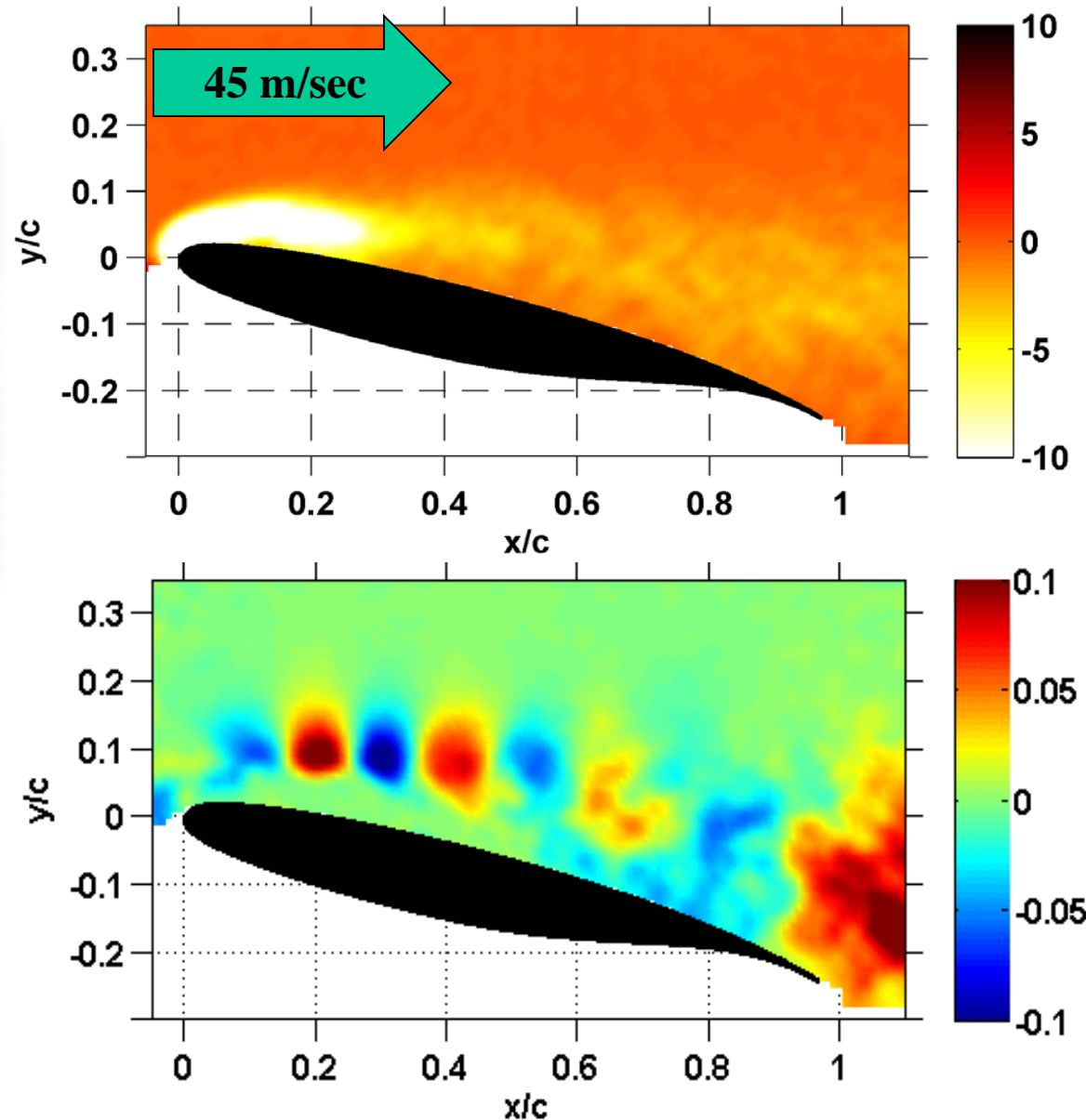


- High amplitude perturbations (localized heating in arc filaments)
- Every discharge pulse results in vortex formation
- Flow responds to forcing near jet column instability frequency

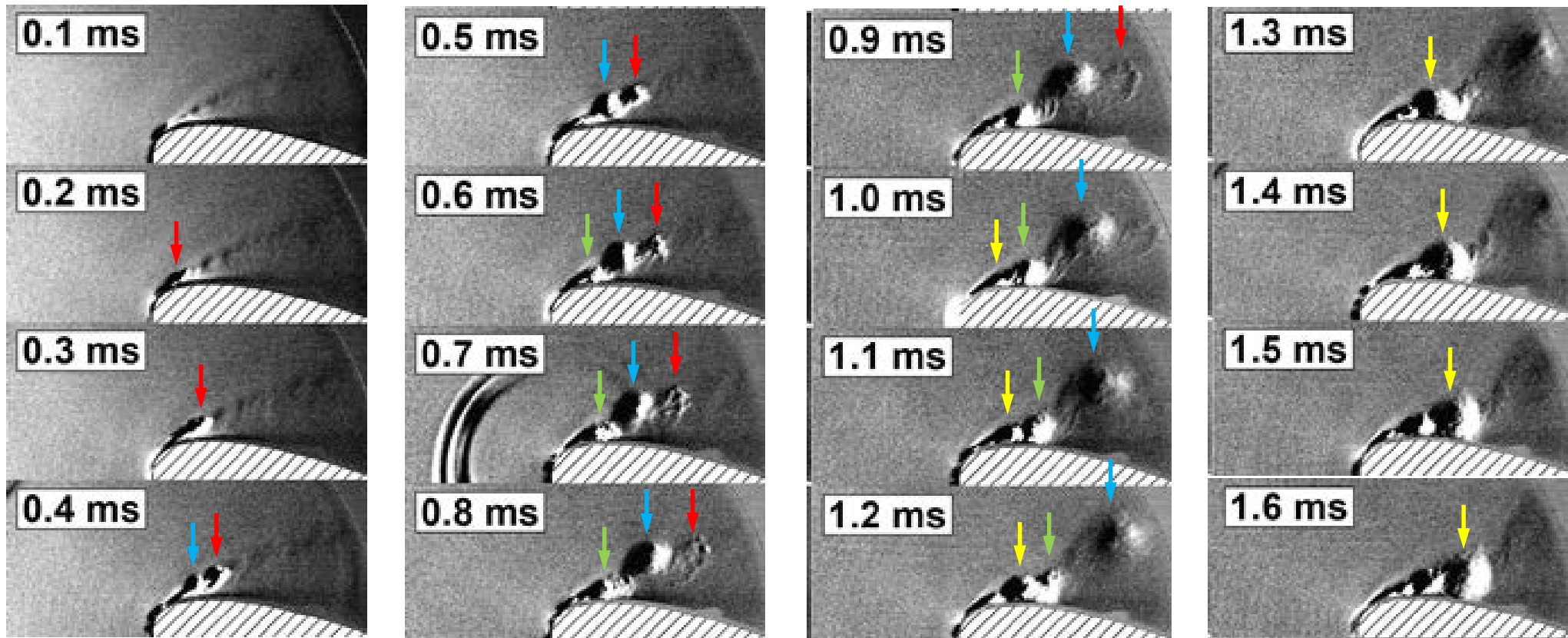
Ns DBD plasma actuators: formation of coherent structures (spanwise vortices)



- Every nanosecond discharge pulse produces a spanwise vortex
- Qualitatively similar to LAFPA actuators
- Enhanced mixing with free stream \rightarrow boundary layer reattachment
- Same effect detected up to $u=96$ m/sec ($M=0.28$, $Re_x \sim 1.5 \cdot 10^6$)



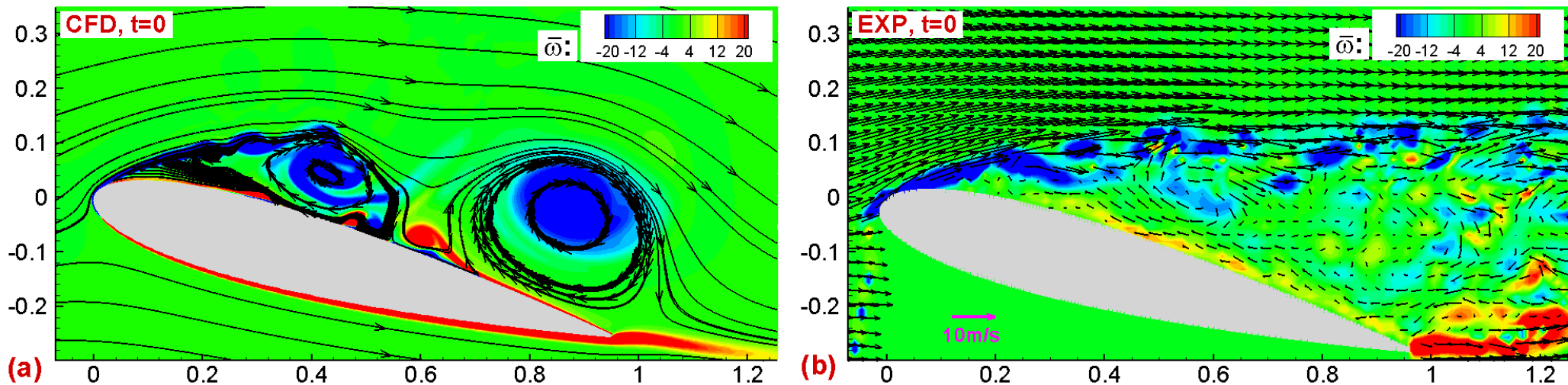
Spanwise vortex dynamics: high-speed schlieren (Tohoku University, Japan)



- $U = 20$ m/s, $AoA = 22^\circ$, $f = 3$ kHz ($\tau = 0.33$ ms)
- Compression waves are seen in **0.7 ms** image only, others are “between the frames”
- No evidence of compression wave on flow structure (compare images at **0.6 ms** and **0.7 ms**)
- Every discharge pulse generates an individual vortex, all vortices appear to rotate clockwise
- Vortices **#1** and **#2** travel above the separation zone, all subsequent vortices follow the surface

PIV measurements and plasma / CFD modeling: (National University of Singapore, AIAA Papers 2017-0712, 0715)

- Objective: obtain quantitative insight into the mechanism of plasma flow control

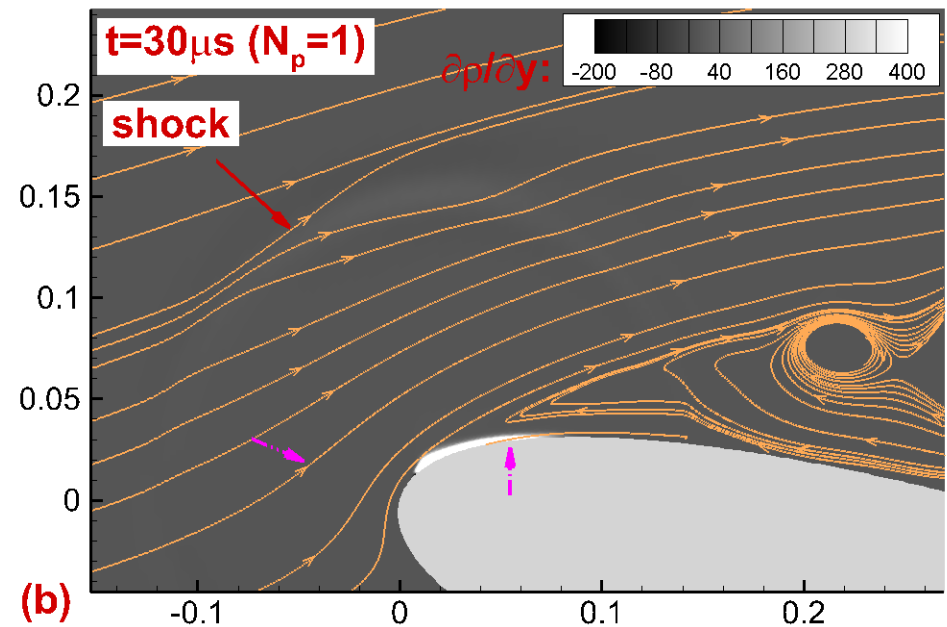
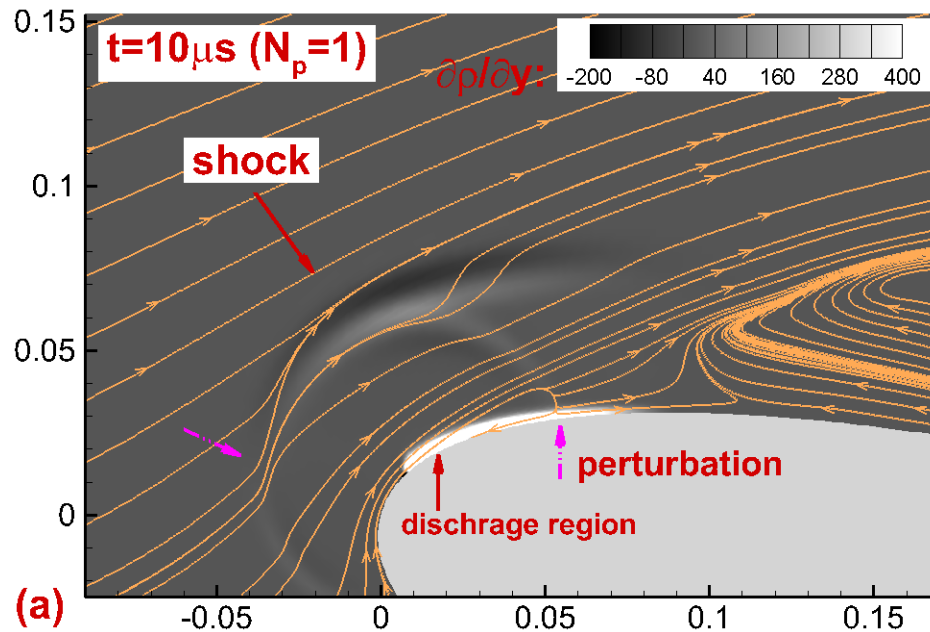


Baseline flow (without control): $Re = 0.05 \cdot 10^6$ ($U_\infty = 10$ m/s), $AoA = 15^\circ$

Ns pulse surface ionization wave plasma / volumetric residual heating model
(Takashima et al., Plasma Sources Sci. Technol. 2013)

Coupled with 2-D compressible flow Navier-Stokes equations

Are spanwise vortices formed by compression waves?



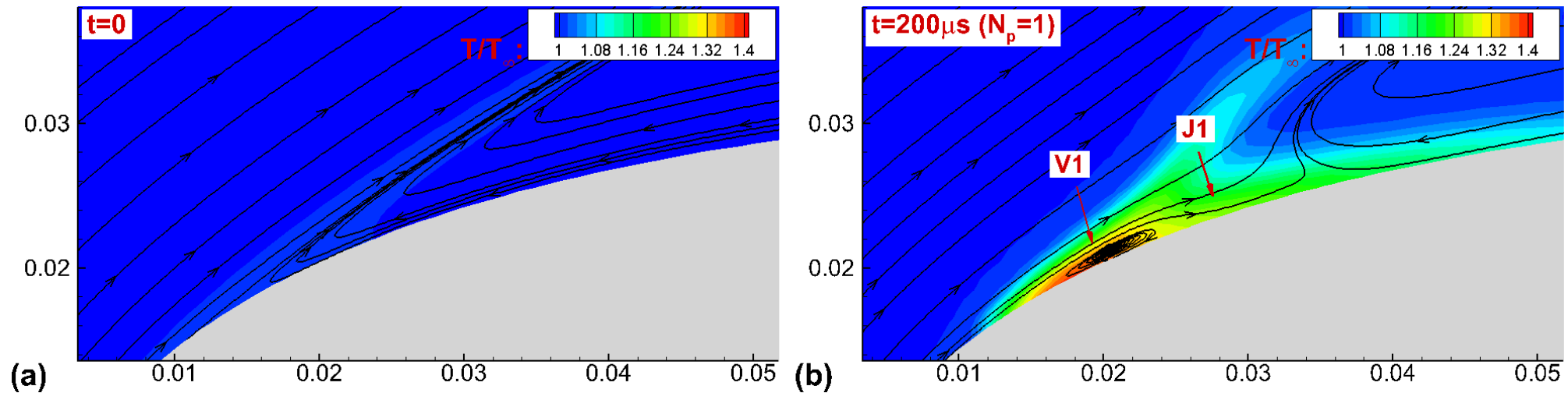
Numerical schlieren images overlaid with streamlines:

Compression wave propagation through the external flow

$\text{Re} = 0.05 \cdot 10^6$ (10 m/s), $\text{AoA} = 15^\circ$, $U_p = 20$ kV, $f = 0.15$ kHz, $f^+ = 1.2$

Effect of compression wave on external flow is very weak

Are spanwise vortices formed by residual heating?



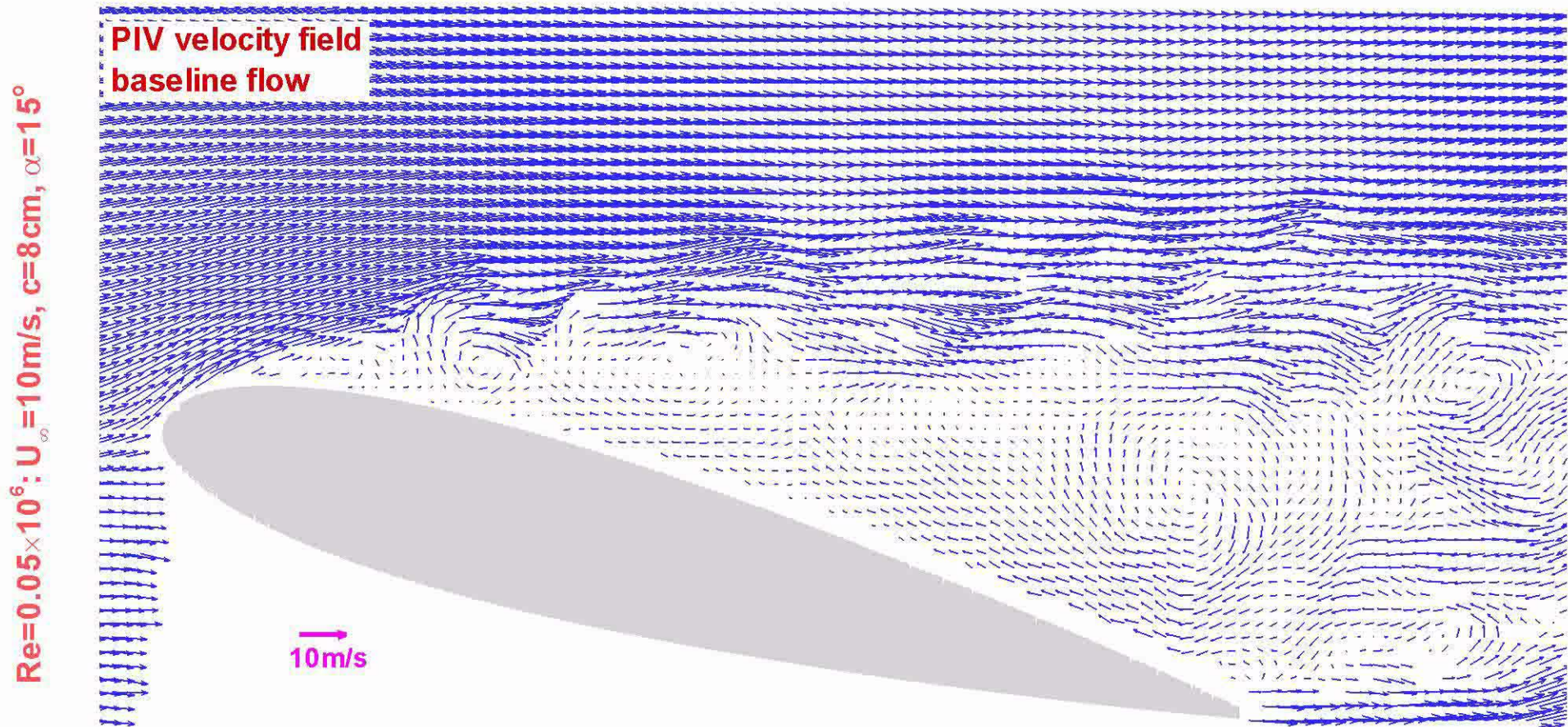
Numerical schlieren images overlaid with streamlines:

$Re = 0.05 \cdot 10^6$ (10 m/s), $AoA = 15^\circ$, $U_p = 20$ kV, $f = 0.15$ kHz, $f^+ = 1.2$

**Generation of a spanwise vortex by residual heating
after the first discharge pulse (via inviscid instability)**

Experimental (PIV) data

Baseline and forced flows, $Re = 0.05 \cdot 10^6$

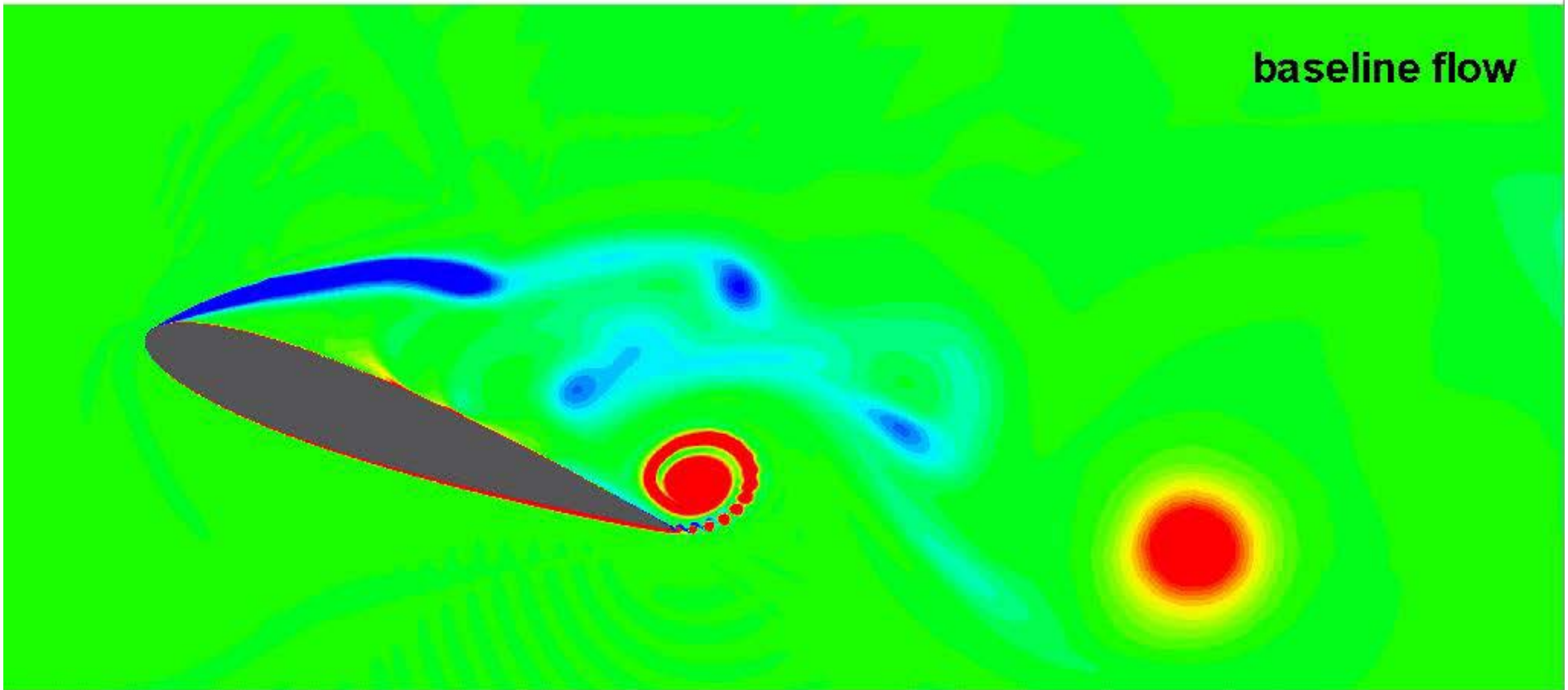
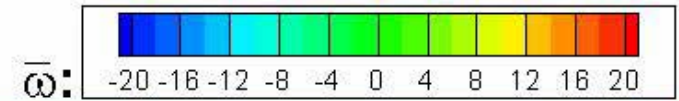


Spanwise vortex formation, flow reattachment begins after the first discharge pulse

Plasma / CFD predictions

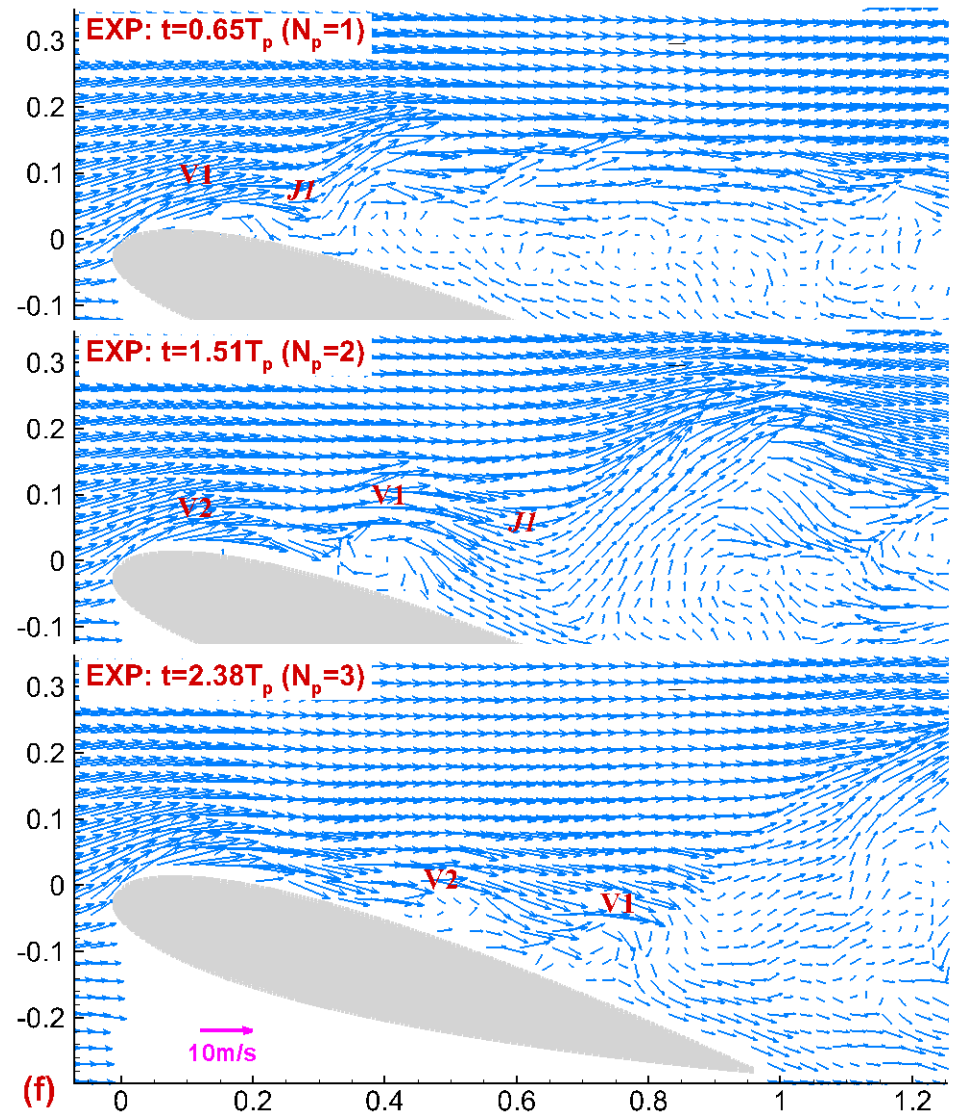
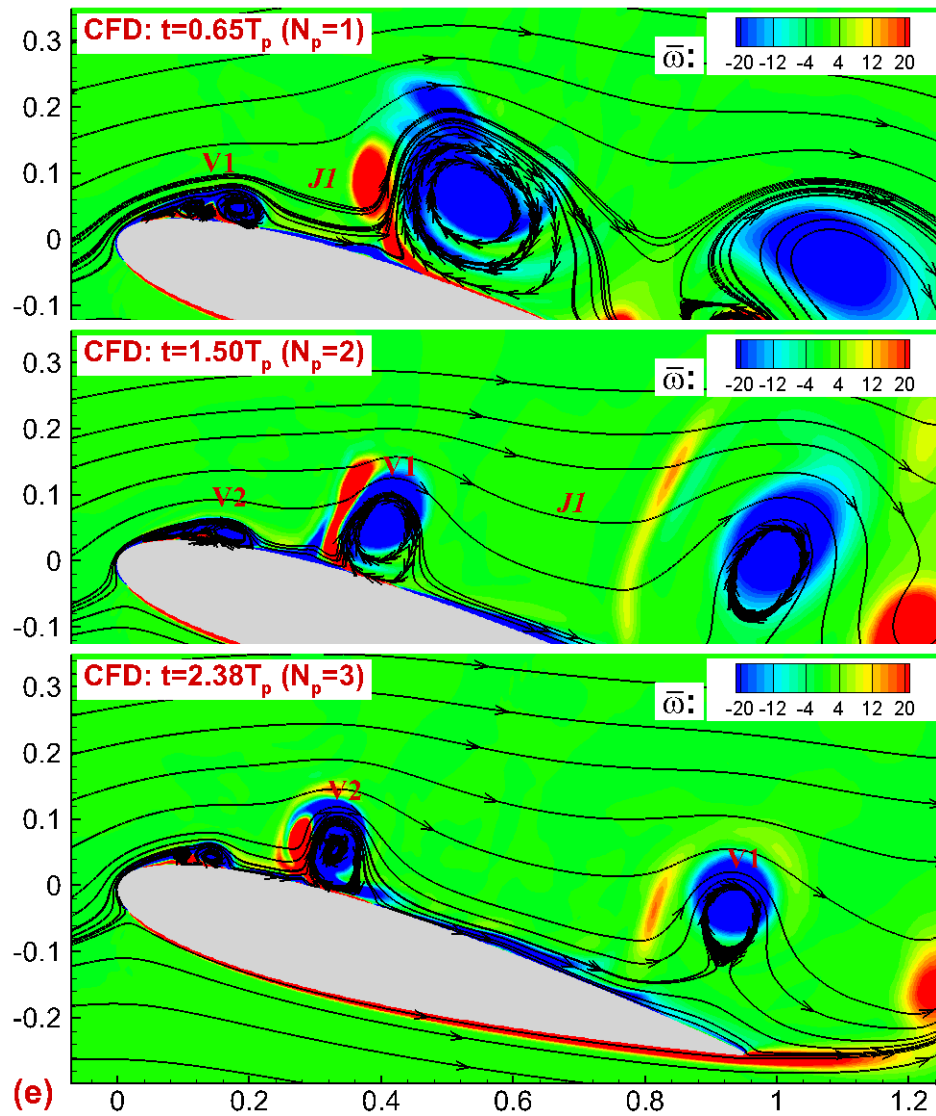
Baseline and forced flows, $Re = 1.2 \cdot 10^6$

$Re = 1.2 \times 10^6$: $U_\infty = 93 \text{ m/s}$, $c = 20.32 \text{ cm}$, $\alpha = 20^\circ$



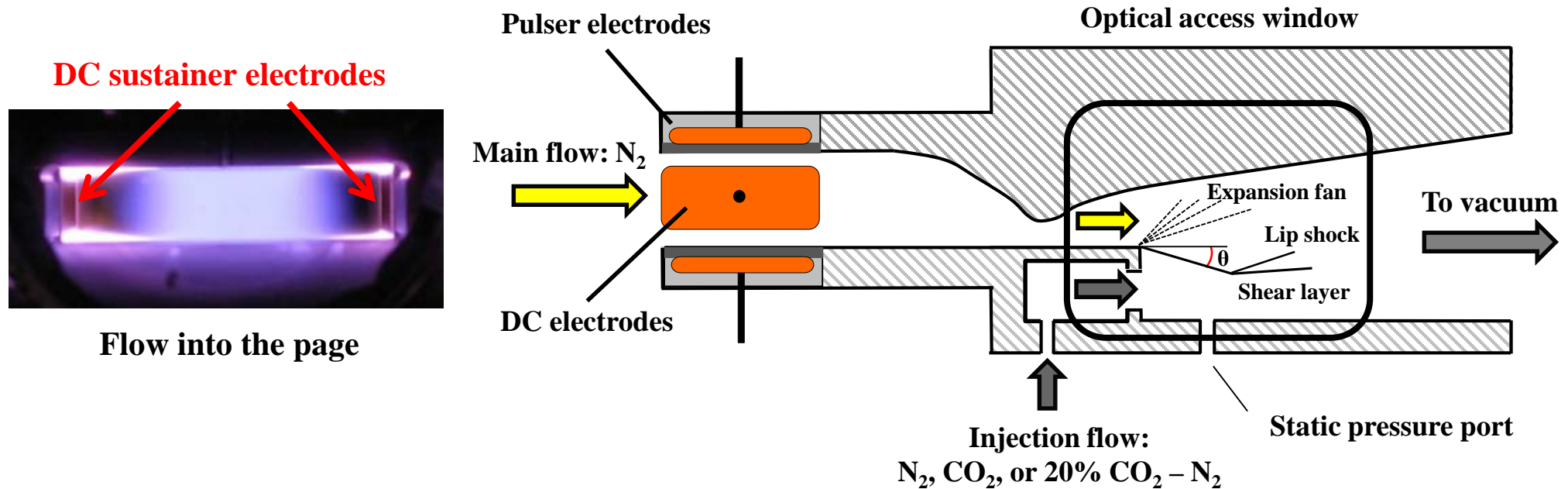
Residual heating after every discharge pulse results in a spanwise vortex formation

Comparison between PIV data and CFD predictions: $Re = 0.05 \cdot 10^6$



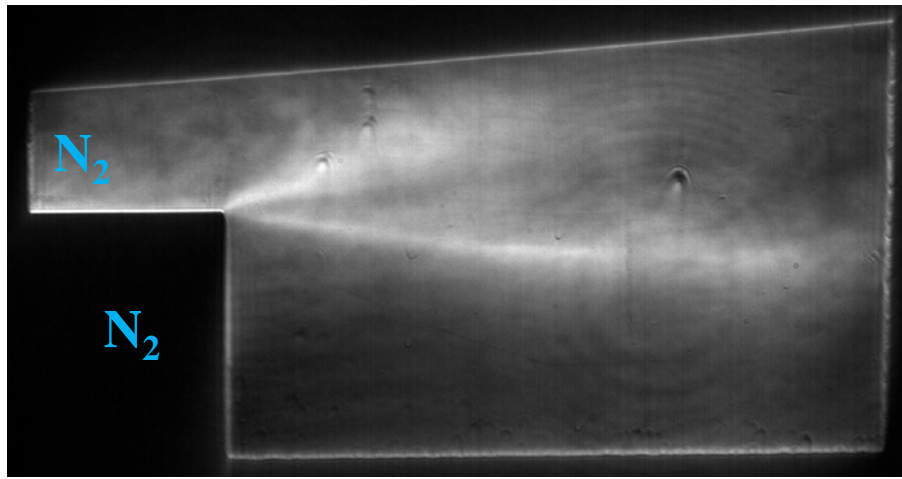
Results compared after $N_p = 1, 2$, and 3 discharge pulses: good qualitative agreement

Using accelerated relaxation of vibrational energy to control supersonic mixing / shear layer

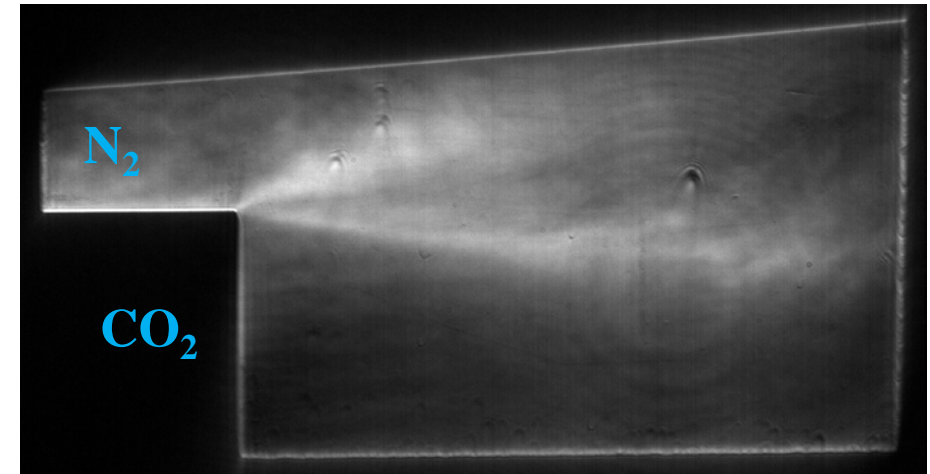


- Plenum: overlapped ns pulse / DC sustainer discharge for vibrational loading of N_2
- $P_0 = 300$ torr, $T_v = 2000$, $T = 500$ K, 2-D nozzle, top wall contoured, bottom wall plane
- Condition at nozzle exit : $M = 2.5$, $P_{exit} = 15$ torr
- Subsonic flow below expansion corner: injection of N_2 or CO_2
- Optical access for schlieren, CARS, and NO PLIF in subsonic and supersonic flows

Effect of vibrational relaxation of shear layer: N_2 / N_2 (left) vs. N_2 / CO_2 (right)



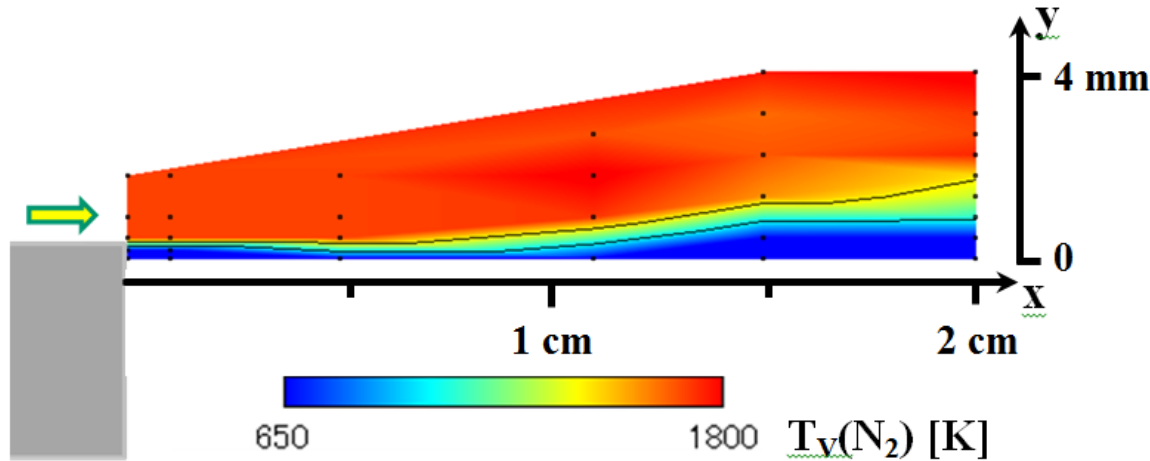
N_2 “bleeding” through backstep



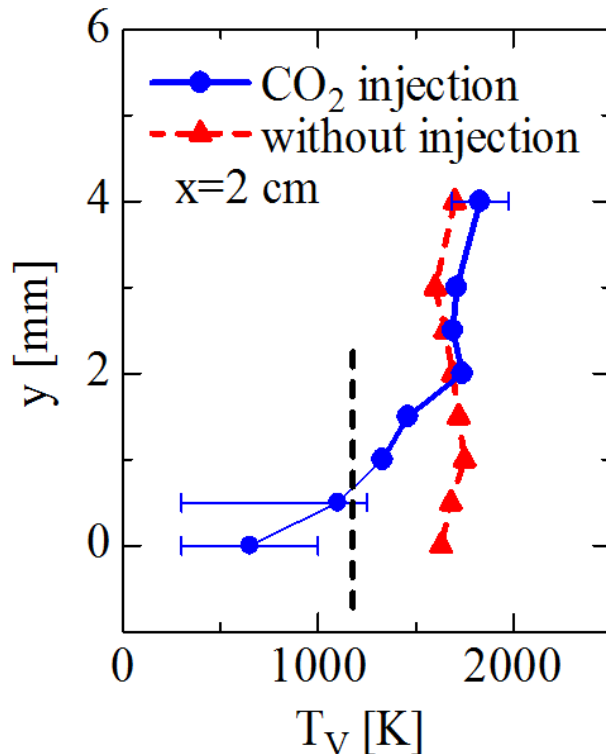
CO_2 “bleeding” through backstep

- Time delay between frames 5 ms, $t = 0-80$ ms
- N_s pulse / DC discharge (2.3 kW) is turned on at $t = 10-45$ ms, to excite main N_2 flow
- No perturbation of shear layer detected in N_2 / N_2 flow
- In N_2 / CO_2 flow, shear layer expansion angle decreases, approaching $\theta=0^\circ$
- No change observed if main N_2 flow is not excited

N₂ Vibrational Temperature Distribution in Shear Layer



- Top flow: vibrationally excited N₂, T_v=1900 K, estimated T_{rot}=240 K
- Bottom flow: CO₂ bleeding through backstep, static pressure 7 torr



- CO₂ bleeding reduces T_v(N₂), increases T_{trans/rot} and static pressure
- Consistent with time-resolved measurements in ns pulse discharge in quiescent N₂-CO₂
- Static pressure increase pushes up shear / mixing layer

Nishihara et al, AIAA Paper 2016-1762

Frederickson et al, Plasma Sources Sci. Technol., 2017

Summary

- **Surface and volumetric ns pulse discharges:**
 - Rapid energy thermalization on sub-acoustic time scale, high-amplitude compression wave generation
 - Residual heating affected by slow energy thermalization dominated by vibrational relaxation
 - Kinetics of energy thermalization (“rapid” and “slow” heating) is well understood
 - Dynamics of small-scale random perturbations, their potential for flow control remain uncertain
- **NS-DBD surface plasma actuators**
 - Compression waves have almost no effect on the external flow
 - Large-scale coherent flow structures (spanwise vortices) are formed by localized residual heating, via inviscid instability
 - Significant flow control authority in subsonic flows (up to $M = 0.3$), scalable to large dimensions (~ 1 m)

Summary (cont.)

- **Flow control by accelerated vibrational relaxation:**
 - Injection of “relaxer” species in nonequilibrium flow
 - Temperature and pressure rise due to accelerated relaxation
 - Strong effect on supersonic shear layer
- **Outstanding issues:**
 - Can “late” small-scale random perturbations be used for boundary layer flow tripping (e.g. see Yan and Gaitonde, Phys. Fluids 2010)?
 - Can accelerating vibrational relaxation (e.g. by CO₂ injection) enhance NS-DBD actuator flow control authority?

Acknowledgments

AFOSR BRI “Nonequilibrium Molecular Energy Coupling and Conversion Mechanisms for Efficient Control of High-Speed Flow Fields”

US DOE Plasma Science Center “Predictive Control of Plasma Kinetics: Multi-Phase and Bounded Systems”

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